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Cost to benefit ratio of an exhaust heat recovery system on a long haul truck

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Abstract

Nearly 30 percent of the fuel energy in an internal combustion engine is lost as waste heat in the form of hot exhaust gases. Nowadays it seems clear that the heavy duty manufacturers will implement bottoming Rankine cycles to recover the exhaust heat on their long haul trucks in the 2020s as an answer to future stringent regulations and the still increasing customer pressure for reductions in operating costs. Though the potential of exhaust heat recovery is clear, the technology has to prove the business, durability and safety cases to be widely spread in the next decade. This paper focuses on the business case of such a technology.

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Keywords: "Heavy duty trucks, exhaust heat recovery, piston expander, fuel saving, cost, business case"

1. Introduction

To date, emission regulations focusing on local pollutants have not focused on the efficiency of internal combustion engines (ICE). However, future regulations will focus on CO_2 emissions, requiring high efficiency increase of the whole drivetrain. The best efficiency of a modern ICE will remain below 42% and research projects tend to increase it up to 50 or 55%. Electrification of ancillaries and hybridization seem to lead to little fuel savings on Heavy Commercial Vehicles (HCVs) and, at least, would be too expensive to reach future CO_2 emissions regulation compared to air drag reduction and waste heat recovery (WHR). While HCVs aerodynamic is mostly constrained by regulation and also depends on trailer manufacturers, WHR appears as essential in the future innovation panel for HCVs. Though the potential of WHR is clear, the technology has to prove the business,

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durability and safety cases to be launched in mass production. This paper is dedicated to assess the business case of such a system through the calculation of the cost of the system and of its payback time. We try to go deeper in details than previous papers did [1].

| Nomen | clature |
|-------|-------------------------------|
| EAT | Exhaust After Treatment |
| HCV | Heavy Commercial Vehicle |
| ICE | Internal Combustion Engine |
| ORC | Organic Rankine Cycle |
| SCR | Selective Catalytic Reduction |
| WHR | Waste Heat Recovery |

2. ORC architecture



Fig. 1. ORC system considered for this business case (turbocharger is not shown)

The truck engine architecture chosen is a so-called "SCR- only" exhaust after-treatment system. Though it is not the best configuration for WHR [2], it has been chosen based on our current development of a demonstration truck. The waste heat is only recovered from the tailpipe as there is no EGR on this engine. The Organic Rankine Cycle (ORC) recovers the heat from the exhaust gases to convert it into mechanical power re-injected on the driveline. In the scheme considered (Fig. 1), there is no electric component: only pneumatic valves for the three of them and mechanical coupling for the two pumps and the expander. The working fluid, which is a mixture containing mostly ethanol, is moved to an evaporator (5) by means of a pump (12). The pump is assumed to be a gear pump. The flow is controlled by means of a liquid bypass valve (15) that re-circulates part of the liquid to achieve the desire superheating at the evaporator outlet. The vapor circulates from the evaporator to the expander (9) that will expand it and will re-inject torque. The expander considered is based on a swashplate architecture counting three pistons cumulating around 240 cm³. This device is coupled to the ICE though the gear of an engine PTO. We assume a simple passive freewheel and a damping system between the expander shaft and the PTO gear. A vapor bypass valve (8) may help the warm-up the expander or the stop of the ORC. The vapor at low pressure goes to a condenser (10) that is cooled in parallel of the existing engine cooling loop. The additional cooling pump is mechanically linked to the engine. The working fluid which has been condensed is pumped back to the evaporator. The evaporator and the condenser are assumed to be plate heat exchanger in stainless steel for temperature and corrosion issues. A gas bypass valve (4) is used to control the load on the ORC and reduce the cooling needs on the radiator to favor the cooling of the main engine.

Though the purpose of the paper is not to detail the fuel savings, we have to make an assumption to assess the payback time. According to [3] with a similar ORC architecture but with a very large evaporator, the fuel saving in a real driving cycle may be assumed to range between 2.6 to 2.9% with possible improvements. On the other hand, a simple static calculation on a design point (in table 1) assuming an evaporator effectiveness of 75% and a pump and expander net isentropic efficiencies of 36% and 55% respectively, gives 3.4% fuel saving. From several papers, we know that the dynamics of the system may reduce this potential by a factor up to 2 [4]. We will then assume 3% $\pm 0.5\%$ fuel savings for the payback time estimation.

| | Value | Unit |
|-----------------------------|-------|---------|
| Engine power | 108 | kW |
| Exhaust massflow | 179 | g/s |
| Exhaust temperature | 331 | °C |
| Exhaust gases specific heat | 1.066 | kJ/kg/K |
| Vapor pressure | 20 | bar |
| Vapor superheat | 30 | °C |
| Condensing pressure | 1 | bar |
| Required pump NPSH | 300 | mbar |

Table 1. Nominal design point and assumption for fuel savings calculation.

3. Costing method

Table 2 Sales scenario

To assess the cost of such a system we first need an assumption on the yearly sales in order to figure out the type of manufacturing process, from an integrated approach with machining in-house and a fully automated assembly line to an out-sourced strategy coupled to a manual assembly line. The following sales scenario that gives a cumulated number of 250,000 pieces over 8 years will direct us to the second strategy. The forecast volumes are too low to justify a high level of integration and automation.

| | Y1 | Y2 | Y3 | Y4 | Y5 | Y6 | Y7 | Y8 |
|-------------------------|-------|--------|--------|--------|--------|---------|---------|---------|
| Sales per year (unit/y) | 5 000 | 10 000 | 15 000 | 25 000 | 32 500 | 42 500 | 52 500 | 67 500 |
| Cumulated sales (units) | 5 000 | 15 000 | 30 000 | 55 000 | 87 500 | 130 000 | 182 500 | 250 000 |

The costing method will then consist in detailing all the parts of each component and calculate a cost for each. The sum of it will give the "purchased parts and services". Some details of the cost breakdown can be found in Appendix A. They are sum up in table 2. The cost calculation method of the parts may vary from a rough estimation based on our experience or from a quotation from suppliers, to a calculation based on the weight and the material cost of the part. For instance, the latter pattern is applied for the plates of the heat exchangers that are in stainless steel. We assume $3.6\epsilon/kg$ for the material. The weight is calculated based on the size of the part and the density of the material. Last, we add an extra factor of 1.4 to cover all expenses related to material wastes, machine rate, etc.

In addition to this cost, we add the tooling and assembly investment costs. Regarding the plates of the heat exchanger we assume a process of stamping with a tool at 300,000. The plates are then manually assembled to form a stack which is pressed while the fittings are positioned by an assembly machine. Then the stack is brazed in a furnace, before being tested under pressure. This process gives us three assembly machines which costs are gathered into the 1,000,000€. These investment costs are divided by the cumulated number of sales over 8 years to form the cost added per part.

The labor to assemble the components is accounted as follow. We take a rate of $40\epsilon/h$ plus a 1.2 factor to account for the overheads. We multiply this rate by an estimation of the assembly duration. The cost includes all commodities: buildings, electricity...

A ratio of 30% on the sum of all previous costs is taken to account for the SG&A and the profit that should cover the R&D costs as well as the expected return on investment.

The sum of all these costs gives the manufacturing cost of the components. Then we add the margin of the OEM to integrate the system and cover the R&D costs. The margin is accounted as a percentage of $+80\%\pm20\%$ based on the component costs.

4. System cost

It can be seen that the total weight of the system is estimated at \sim 110kg, the half of which is coming from the exhaust evaporator (including the extra weight of the caning of the EAT).

| Component | Weight [kg] | Main material (if applicable) | Purchase parts and services | Total Toolings | Total Assembly investments | Assembly labor | SG&A & profit | Total |
|--|----------------|----------------------------------|--------------------------------|-------------------|----------------------------------|-------------------|---------------|----------|
| Exhaust bypass valve | 4.2 | Stainless steel | 56.83 € | 600,000€ | 500,000€ | 4€ | 19.57€ | 84.80 € |
| Exhaust evaporator | 46.6 | Stainless steel | 321.78 € | 600,000€ | 1,000,000€ | 8 € | 99.65€ | 431.84 € |
| Expander, coupling & vapor bypass valve | 15.3 | Cast iron / Steel | 315.00€ | 1,800,000€ | 2,000,000€ | 16€ | 100.26€ | 434.46€ |
| Condenser | 13.8 | Stainless steel | 69.52 € | 600,000€ | 1,000,000€ | 8€ | 23.98€ | 103.90€ |
| Cooling pump | 0.4 | Cast iron / Steel | 19.00 € | 600,000€ | 300,000€ | 4€ | 7.98€ | 34.58 € |
| Piping | 15.4 | - | 52.82 € | 250,000€ | 0 € | 4€ | 17.35€ | 75.17€ |
| Tank system | 2.6 | Plastic | 56.00 € | 300,000€ | 300,000€ | 8 € | 18.72€ | 81.12 € |
| Fluids | 8.6 | - | 20.00 € | 0€ | 0 € | 0€ | 7.20€ | 31.20 € |
| Feed pump | 0.4 | Plastic / Steel | 41.00 € | 300,000€ | 500,000€ | 4€ | 14.46€ | 62.66 € |
| Control valve | 0.2 | Plastic / Steel / Copper | 22.00 € | 600,000€ | 500,000 € | 4€ | 9.12€ | 39.52 € |
| ECU, harness & sensors | 2.5 | - | 58.00 € | 0€ | 0€ | 0€ | 18.60€ | 80.60 € |
| Total | 110 kg | - | 1,032 € | 5,650,000€ | 6,100,000€ | 60€ | 342€ | 1,481€ |

Table 3. Component costs.

In Fig. 2 (left), a pie chart illustrates the cost breakdown showing that 60% of the cost is resulting from the evaporator and the expander costs. Adding the OEM margin, it gives us a total system cost around $2,666 \pm 296 \in$.



Fig. 2. Left: ORC manufacturing cost breakdown. Right: Requirements for a payback time of two years in different world regions

5. Payback time estimation

To assess the payback time, we defined three regions with homogenous parameter in terms of truck use: Europe, the USA and China. These parameters are gathered in table 3. The figure for the Chinese truck consumption is a forecast after the implementation of the "China 6" regulation that should be set up between 2019 and 2025. The mileage for Chinese truck is an average between express delivery, coal delivery or refrigeration trucks. For the USA trucks, we took the class 8 truck averages for mileage and consumption coming from the U.S. department of Energy [5]. Other figures come from our customer feedbacks.

| ruore in rissumptions for purjouent time europaution. | | | | | | | | |
|---|---------|---------|---------|---------|--|--|--|--|
| | Europe | USA | China | Unit | | | | |
| Mileage | 130,000 | 110,000 | 150,000 | km/y | | | | |
| Fuel | 1 | 0.65 | 0.8 | €/L | | | | |
| Consumption | 35 | 44 | 35* | L/100km | | | | |
| ORC Maintenance | 100 | 100 | 100 | €/y | | | | |

*: projected in 2025 with new regulation implementation

Table 4 Assumptions for payback time calculation

In Fig 2 (right), we plot the line that allows reaching a 2 year payback period on the ORC given its sales prices and its associated fuel savings.

As a result, it can be seen that the business case of the system can be met in Europe or in China whereas in the USA the diesel price makes it very difficult. There, only a CO_2 regulation, for example the Phase 2 Greenhouse Gas Emissions and Fuel Efficiency Standards set by the EPA and NHTSA [6], could help the market penetration.

6. Conclusion

Waste heat recovery on long haul trucks is the future technology to reduce fuel consumption. This paper tries to establish that such systems can meet the stringent requirements to make a strong business case. It has been proved that though a 2 year payback time may be considered, future improvements are requested to decrease costs and increase efficiency at least for the USA market. As an expander developer, the Exoès company answers this challenge in two folds. First is to design cost effective solutions integrating functions, reducing the quantity of parts and reducing the use of expensive materials in the expander. Second is to improve the expander efficiency, which is key in the system performance, with the target to reach 65-70% effective isentropic efficiency.

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Appendix A. Detailed sub-components costs and characteristics

| | | | | Woight | Tooling | Unit cost | Total Cost | Total woight |
|---|--|---------|------------------------|--------|-----------|-------------|----------------|--------------|
| Category | Parts | Qty | Main material | [kg] | [£] | Iffl | | local weight |
| Exhaust avenageter | Fitting M tube | 1 | stainlass staal | [Ng] | [€] | | | [NG] |
| Exhaust evaporator | Fitting OUT tube | 1 | stainless steel | 0.1 | | 0.4 | 0.4€ | 0.1 |
| Exhaust evaporator | Plate 200x 200mm | 1 60 | stainless steel + clad | 0.1 | 200.000 | 2.4 | 202.2 € | 28.8 |
| Exhaust evaporator | Fiate 300x200mm | 20 | stainless steel + clad | 0.5 | 300 000 | 2.4 | 203.2 € | 14.4 |
| Exhaust evaporator | Extra caping EATS 200x200mm | 30 | stainless steer + cidu | 2.3 | 300 000 | 5.4 16.1 | 101.0€ | 2.2 |
| Exhaust evaporator | Extra caring EATS 500X200X200IIIII | 1 | stainless steel | 0.5 | 200.000 | 2.5 | 256 | 3.2 |
| Exhaust bypass valve | | 1 | stainless steel | 0.5 | 300 000 | 0.1 | 2.J€ 01£ | 0.5 |
| Exhaust bypass valve | Bushing | 2 | carbono | 0.0 | | 2.0 | 0.10 | 0.0 |
| Exhaust bypass valve | Busining Desumption actuator with position concor | 1 | Carbone | 0.1 | | 2.0 | 4.0€ | 0.1 |
| Exhaust bypass valve | | 1 | - | 0.5 | | 20.0 | 20.0€ | 0.3 |
| Exhaust bypass valve | Din | 1 | stainless steel | 0.0 | | 0.1 | 0.1€ | 0.0 |
| Exhaust bypass valve | FIII Seat D100 | 1 | stainless steel | 0.0 | 200.000 | 15.1 | 1516 | 0.0 |
| Exhaust bypass valve | Beaumatic selencid valve | 1 | staniess steer | 5.0 | 300 000 | 15.1 | 15.1€ | 3.0 |
| Cooling nump | Casing | 1 | cast iron | 0.5 | 200.000 | 10.0 | 10.0€ | 0.3 |
| Cooling pump | Casilig | 1 | | | 300 000 | 10.0 | 10.0€ | 0.4 |
| Cooling pump | wheel | 1 | cast iron | 0.4 | 300 000 | 3.0 | 3.0€ 2.0€ | 0.0 |
| Cooling pump | Axie | 1 | steel | 0.4 | | 2.0 | 2.0€ | 0.0 |
| Cooling pump | Shaft cool | 1 | steer | | | 2.0 | 2.0€ | 0.0 |
| Coordenser | Sildit Sedi | 1 | elastoniel | 0.7 | 200,000 | 2.0 | 2.0€ | 0.0 |
| Condenser | FIGHT / Dack plate | 1 | stainless steel | 0.7 | 300 000 | 3.0 | 3.0€ | 0.7 |
| Condenser | Filte 100x20011111 | 30 | stainless steel | 0.2 | 300 000 | 1.2 | 126 | 12.0 |
| Condenser | Fitting tube out D12 | 1 | stainless steel | 0.2 | | 1.5 | 1.5€ | 0.2 |
| Condenser | Fitting tube out D12 | 2 | stainless steel | 0.0 | | 0.2 | 0.2€ | 0.0 |
| Condenser | | 2 | Aluminum | 0.4 | 200,000 | 2.0 | 4.0€ | 0.8 |
| Feed pump | Casing | 2 | Aluminum | | 300 000 | 10.0 | 10.0€ | 0.4 |
| Feed pump | Geal | 2 | cast ii uii | 0.4 | | 3.0 | 10.0€ | 0.0 |
| Feed pump | Axie | 2 | steel | 0.4 | | 2.0 | 4.0€ | 0.0 |
| Feed pump | Shaft cool | 4 | steer | | | 5.0 | 12.0€ | 0.0 |
| Control valvo | Silait Seal | 1 | Connor | | 200.000 | 5.0 | 5.0€ 7.0£ | 0.0 |
| Control valve | Coll | 1 | Diastic | | 300 000 | 7.0 | 7.0€ | 0.2 |
| Control valve | Body | 1 | Plastic | | 300 000 | 2.0 | 2.0€ | 0.0 |
| Control valve | Needle | 1 | Steel | 0.2 | | 5.0 | 5.0€ | 0.0 |
| Control valve | Spring | 1 | Stool | 0.2 | | 5.0 | 5.0€ | 0.0 |
| Control valve | Soaling | 1 | alastomor | | | 1.0 | 1.0€ | 0.0 |
| Control valve | Buching | 1 | Stool | | | 2.0 | 2.0€ | 0.0 |
| Piping | HP HT 2m pipe + flexible base + 2 fittings | 1 | Stainloss staal | 1 / | 50,000 | 3.0 | 3.0E | 1.4 |
| Piping | HD LT 1m pipe + nextble hose + 2 httings | 1 | Elactomor | 0.2 | 50 000 | 7.2 | 7.2€ | 1.4 |
| Piping | IP LT 2m pipe + nipples | 1 | Elastomer | 0.3 | 50,000 | 5.0 | 5.0€ | 0.3 |
| Pining | | 1 | Elastomer | 0.3 | 50 000 | 10.0 | 5.0€ 10.0€ | 0.3 |
| Pining | Cooling D50 iron tube 5m | 1 | Steel | 13.1 | 50 000 | 25.6 | 25.6€ | 13.1 |
| ECII barness & sensors | Brossure + temperature sensor | 2 | 51001 | 0.2 | 50 000 | 6.0 | 12.0 € | 0.6 |
| ECU, harness & sensors | | 2 | | 0.3 | | 4.0 | 12.0€ | 0.0 |
| ECU, harness & sensors | Harness | 1 | | 1.0 | | 4.0 | 10.0€ 15.0€ | 1.0 |
| FCI1 harness & sensors | FCI | 1 | _ | 0.5 | | 15.0 | 15.0€ 15.0€ | 0.5 |
| Tank system | | 1 | Aluminum | 0.5 | | 7.0 | 13.0€ | 0.5 |
| Tank system | Low pressure + cafety tank | 2 | Plastic | 1.0 | 200.000 | 15.0 | 20.0€ | 2.0 |
| Tank system | | 1 | Flastic | 0.2 | 300 000 | 10.0 | 30.0€ | 2.0 |
| Tank system | Pressure control solenoid valve | 1 | Liastoniei | 0.2 | | 4.0 | 4.0€ 15.0£ | 0.2 |
| Eluide | Ethanol96% + Denaturant 10 | 1 | - | 0.5 | | 15.0 | 15.0€ | 0.5 |
| Fluids | Lubricant 500ml | 1 | - | 0.0 | | 5.0 | 10.00 | 0.0 |
| Expander coupling % | | T | - | 0.0 | | 5.0 | 3.UE | 0.0 |
| vapor bypass valve | Expander + bypass valve + coupling | 1 | - | 15.0 | 1 800 000 | 300.0 | 300.0€ | 15.0 |
| Expander, coupling & vapor bypass valve | Pressure control solenoid valve | 1 | - | 0.3 | | 15.0 | 15.0€ | 0.3 |